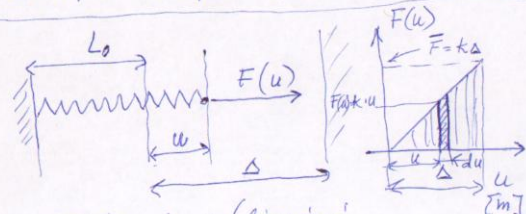
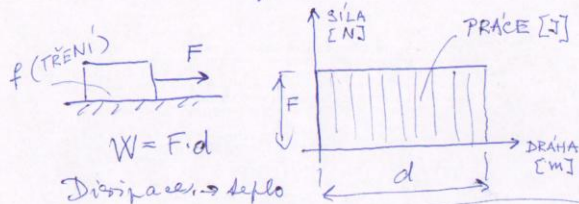
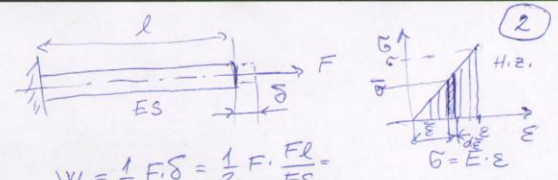
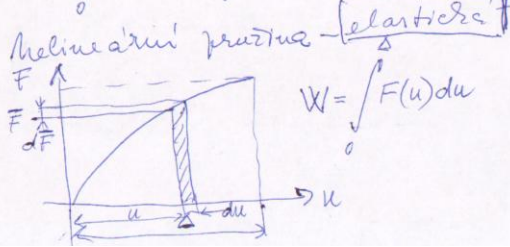


Teor. jako metoda z počít z PPI metoda z rovnic z PPI
 započít se už: práce v daném 2. o. oba.
 práce může být síla



nelineární pružina (elastická)

$W = \int_0^{\Delta} F(u) du$



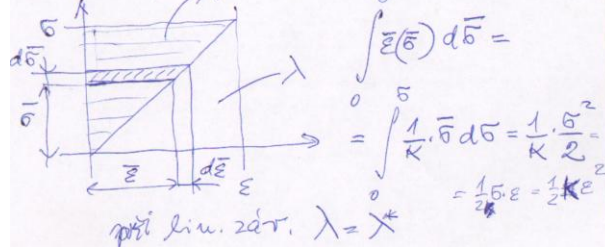
\rightarrow v deformované tělo je práce mezi silou vložená jako def. en. uvolní se při odlehu.

$U = W$
 Hustota deformační energie (na jednotku objemu)
 $\lambda = \frac{U}{V} = \frac{1}{Sl} \cdot \frac{1}{2} \frac{F^2 l}{ES} = \frac{1}{2E} \left(\frac{F}{S}\right)^2 = \frac{1}{2} \frac{\sigma^2}{E}$
 $= \frac{1}{2} \sigma \cdot \epsilon \rightarrow$ plocha v zatěž. diagr.
 $\lambda = \int_0^{\epsilon} \sigma d\epsilon = \int_0^{\epsilon} E \cdot \epsilon d\epsilon = \frac{1}{2} E \cdot \epsilon^2$
 $U = \int \lambda dV$

Elastický nelineární materiál

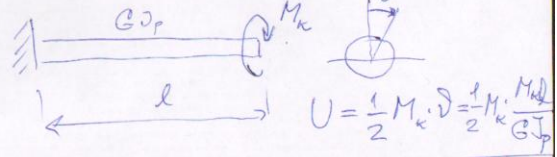
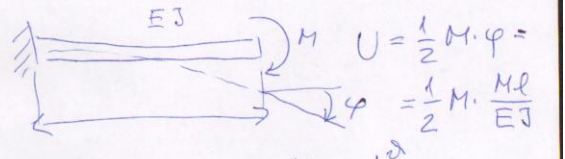
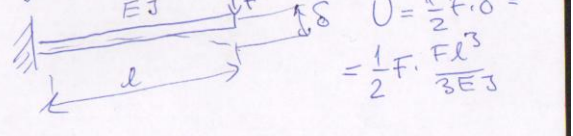
$\lambda = \int_0^{\epsilon} \sigma d\epsilon = \int_0^{\epsilon} k \cdot \epsilon^{\frac{1}{2}} d\epsilon = \frac{2}{3} k \cdot \epsilon^{\frac{3}{2}} = \frac{2}{3} \sigma \cdot \epsilon$

Komplementární deformační energie



$\sigma = k \cdot \epsilon^{\frac{1}{2}}$
 z přídel.
 $\lambda = \frac{2}{3} \sigma \cdot \epsilon$
 $\lambda^* = \sigma \cdot \epsilon - \frac{2}{3} \sigma \cdot \epsilon = \frac{1}{3} \sigma \cdot \epsilon$

Podobně bychom mohli stanovit deformační energii v měřitelích jednodušších případech



Deformační energie u současně typů dlouhých stěhových těl zatížených rovinnou a kruhou

lineární mater. $\lambda = \frac{1}{2} \sigma \cdot \epsilon$
 $\lambda = \frac{1}{2} \sigma \cdot \epsilon$

Tah O.K. (5)

$$U = \int_{(x)} \left(\int_{(s)} \sigma(s) ds \right) dx = \int_{(x)} \left(\int_{(s)} \frac{\sigma(x)^2}{2E} ds \right) dx =$$

$$\frac{1}{2E} \int_{(x)} \frac{N(x)^2}{S} dx \quad \sigma(x) = \frac{N(x)}{S} \quad \int_{(s)} ds = S$$

Ohyb

$$U = \frac{1}{2E} \int_{(x)} \left(\int_{(s)} \left(\frac{M(x)}{J_y} \cdot z \right)^2 ds \right) dx = \int_{(x)} z^2 ds = J_y$$

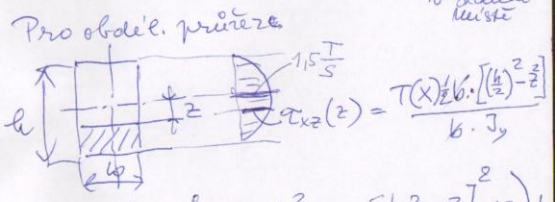
$$= \int_{(x)} \frac{M(x)^2 dx}{2E J_y} \quad \int_{(s)} z^2 ds = J_y$$

Kрут

$$U = \frac{1}{2G} \int_{(x)} \left(\int_{(s)} \left(\frac{M_k(x)}{J_p} \cdot r \right)^2 ds \right) dx = \int_{(x)} \frac{M_k^2(x) dx}{2G J_p}$$

Energie def. od prúche síly u ohybujeje tzei (6)

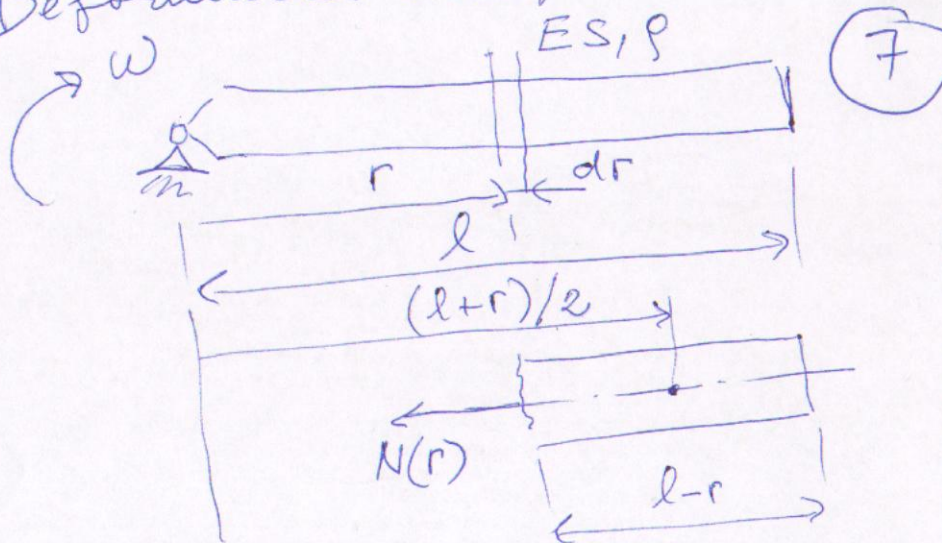
napeti $\sigma_{xz} = \frac{T(x) \cdot \bar{S}_y}{t(x) \cdot J_y}$
 $\bar{S}_y =$ stat. moment oddelené plochy $t(x)$ s t'ím-žeb v dané mieste



$$U_T = \int_{(x)} \left(\int_{(s)} \left(\frac{T(x)}{J_y} \right)^2 \cdot \frac{1}{2G} \left[\left(\frac{h}{2} \right)^2 - z^2 \right] ds \right) dx = \int_{(x)} \frac{24}{4.5} \frac{T(x)^2 dx}{2GS}$$

$\beta = \frac{6}{5} \parallel$
 koef. rozdúlie prúe.

Деформаційна енергія в рот. каміні



$$N(r) = (l-r) \cdot S \cdot \rho \cdot \omega^2 \cdot \frac{(l+r)}{2} \text{ [N]}$$

$$\sigma(r) = \frac{l^2 - r^2}{2} \rho \omega^2 \text{ [Pa]}$$

$$\lambda(r) = \frac{\sigma^2(r)}{2E} \text{ [J m}^{-3}\text{]}$$

$$U = \int_{(V)} \lambda(r) dV = \frac{S}{2E} \frac{\rho \omega^4}{4} \int_0^l (l^2 - r^2)^2 dr = \frac{S \rho^2 \omega^4 l^5}{15E} \text{ [J]}$$

$\frac{K}{U} = \frac{\frac{5}{2} E}{\rho \omega^2 l^2} = \frac{5E}{4 \sigma_{max}}$
 $\frac{K}{U} = \frac{\frac{1}{2} E S}{\rho \omega^2 l^2}$

$dK = \frac{1}{2} \rho S dr (r\omega)^2$
 $K = \int_0^l dK = \frac{1}{2} \rho S \omega^2 \frac{l^3}{3}$

$\sigma_{max} = \frac{1}{2} \rho \omega^2 l^2$
 $kg \cdot m^{-3} \cdot m^2 \cdot s^{-2} \cdot m^3 = N \cdot m$